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Institute for Mathematics, Paderborn University

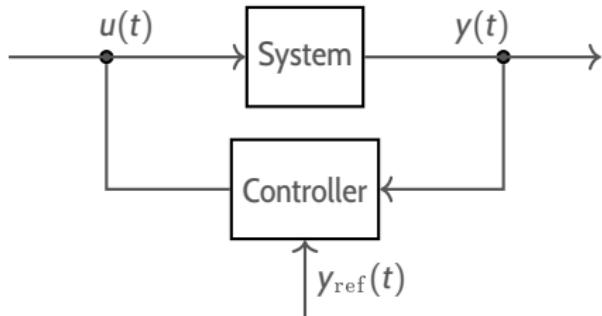
ANALYSIS OF SYSTEM- THEORETIC PROPERTIES OF REAL-WORLD PROCESSES

Thomas Berger

Ilmenau, July 2, 2024



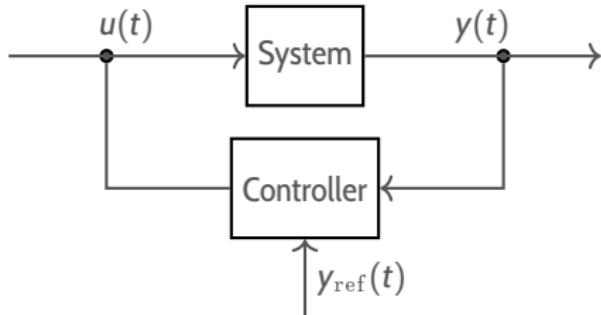
Motivation



$$\begin{aligned}\dot{x}(t) &= f(t, x(t), u(t)), \quad x(t) \in X \\ y(t) &= h(x(t))\end{aligned}$$

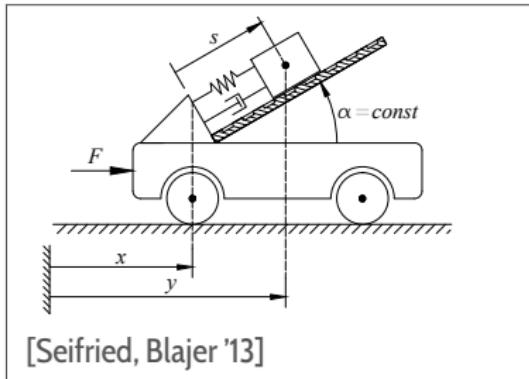
- feasibility of model-agnostic control requires structural properties
- these properties are independent of the dimension of the state space X

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- feasibility of model-agnostic control requires structural properties
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→ **ODEs and PDEs in the same class!**

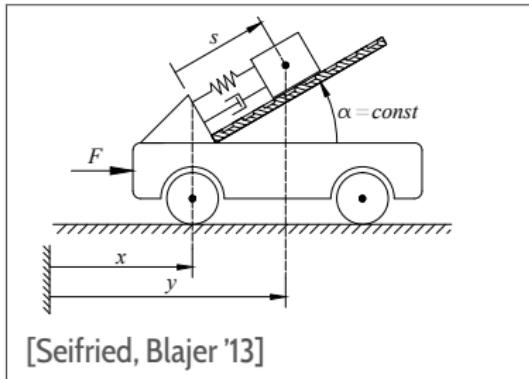


angle: $0^\circ \leq \alpha \leq 90^\circ$

spring, damper with nonlinear characteristics: $K(s)$, $D(\dot{s})$

$$u(t) = F$$

$$y(t) = x(t) + s(t) \cos \alpha$$



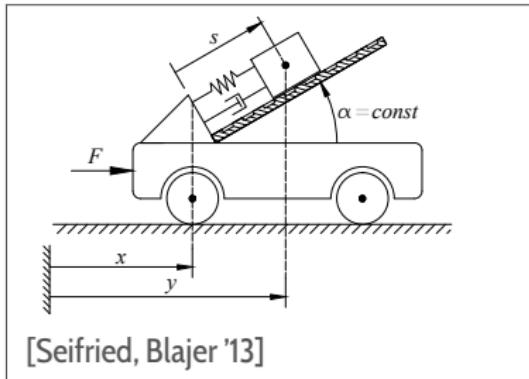
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$$u(t) = F$$

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$$\begin{bmatrix} m_1 + m_2 & m_2 \cos \alpha \\ m_2 \cos \alpha & m_2 \end{bmatrix} \begin{pmatrix} \ddot{x} \\ \ddot{s} \end{pmatrix} = \begin{pmatrix} u \\ -K(s) - D(\dot{s}) + m_2 g \sin \alpha \end{pmatrix}$$



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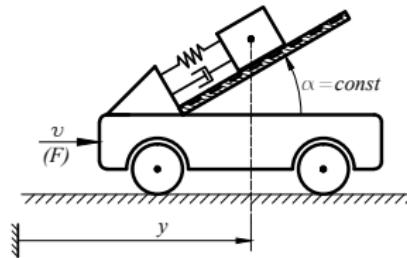
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$$\dot{y} = \dot{x} + \dot{s} \cos \alpha$$

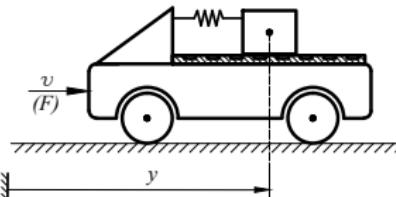
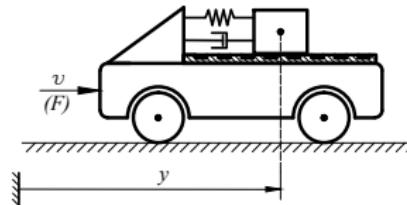
$$\ddot{y} = -c_1(K(s) + D(\dot{s}) - m_2 g \sin \alpha) + \frac{\sin^2 \alpha}{m_1 + m_2 \sin^2 \alpha} u$$

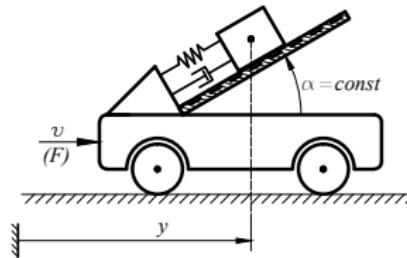


$$0^\circ < \alpha \leq 90^\circ$$

$$\ddot{y} = f_1(s, \dot{s}) + \frac{\sin^2 \alpha}{m_1 + m_2 \sin^2 \alpha} u$$

relative degree = 2

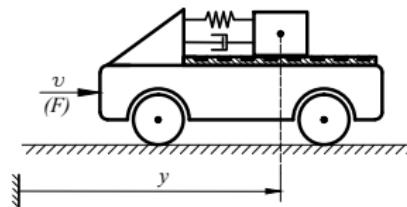




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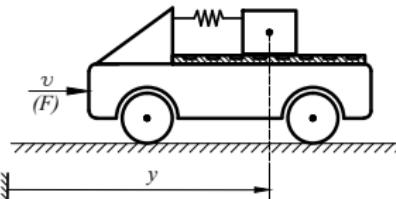
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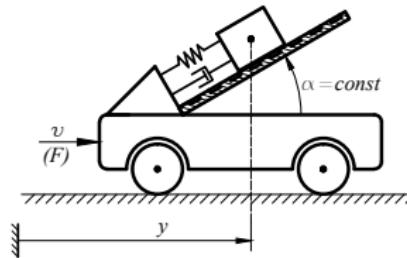


$$\alpha = 0^\circ, \quad D'(\dot{s}) \neq 0$$

$$y^{(3)} = f_2(s, \dot{s}) + \frac{D'(\dot{s})}{m_1 m_2} u$$

relative degree = 3

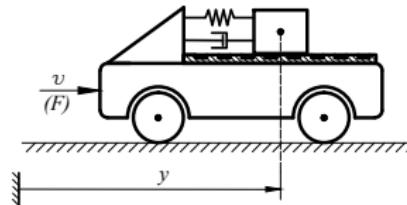




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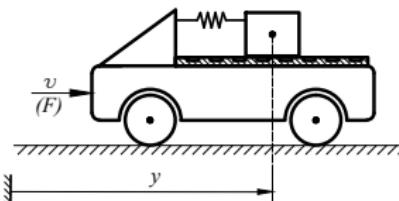
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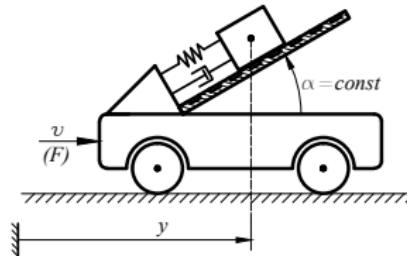
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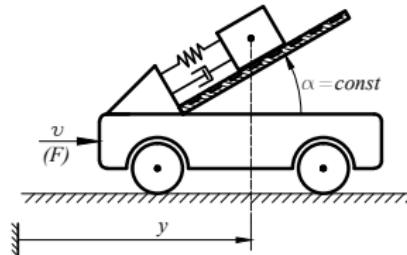
$$\alpha = 0^\circ, \quad D'(\dot{s}) = 0, \quad K'(s) \neq 0$$

$$y^{(4)} = f_3(s, \dot{s}) + \frac{K'(s)}{m_1 m_2} u$$

relative degree = 4

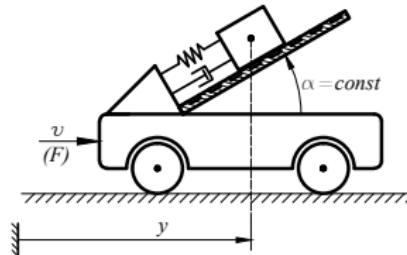


Internal dynamics: remaining dynamics
when output is fixed



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when output is fixed

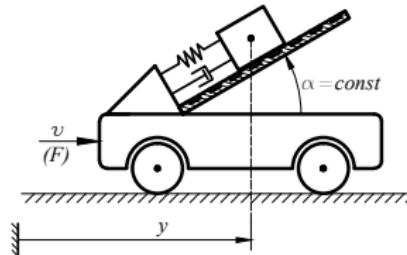
$$\ddot{\eta} = -c_3 K \left(\frac{\eta - y \cos \alpha}{\sin^2 \alpha} \right) - c_3 D \left(\frac{\dot{\eta} - \dot{y} \cos \alpha}{\sin^2 \alpha} \right) + c_4 g \sin \alpha$$



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$$\alpha = 90^\circ, m_2 = 1 : \quad \ddot{s} = -K(s) - D(\dot{s}) + g$$

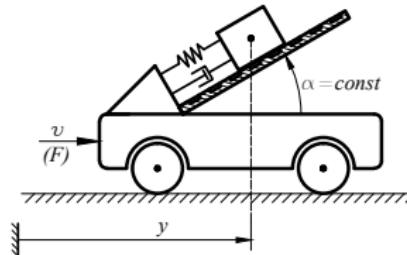


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$$\alpha = 90^\circ, m_2 = 1 : \quad \ddot{s} = -K(s) - D(\dot{s}) + g$$

- Lyapunov function: kinetic + potential energy
- dissipativity: $D(\dot{s})\dot{s} \geq 0$



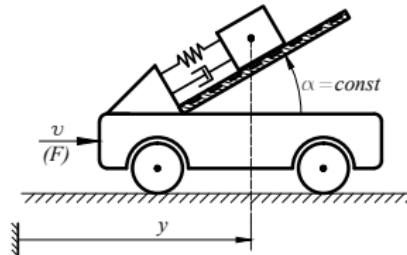
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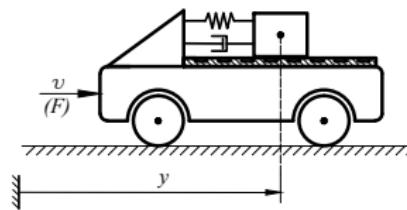
- Lyapunov function: kinetic + potential energy
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$\implies s, \dot{s} \in L^\infty \quad (\text{stable internal dynamics})$



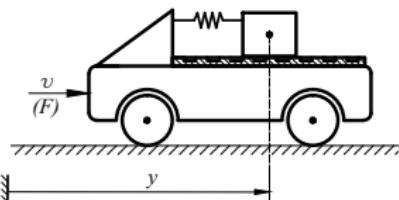
$$0^\circ < \alpha \leq 90^\circ$$

stable internal dynamics



$$\alpha = 0^\circ, \quad D'(\dot{s}) \neq 0$$

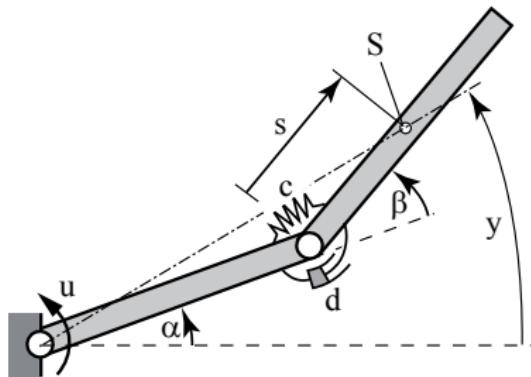
stable internal dynamics



$$\alpha = 0^\circ, \quad D'(\dot{s}) = 0, \quad K'(s) \neq 0$$

no internal dynamics

Rotational Manipulator Arm



$$M \begin{pmatrix} \ddot{\alpha}(t) \\ \ddot{\beta}(t) \end{pmatrix} = \begin{pmatrix} f_1 \\ f_2 \end{pmatrix} + \begin{bmatrix} 1 \\ 0 \end{bmatrix} u(t),$$

$$y(t) = \alpha(t) + \frac{s}{s+l} \beta(t)$$

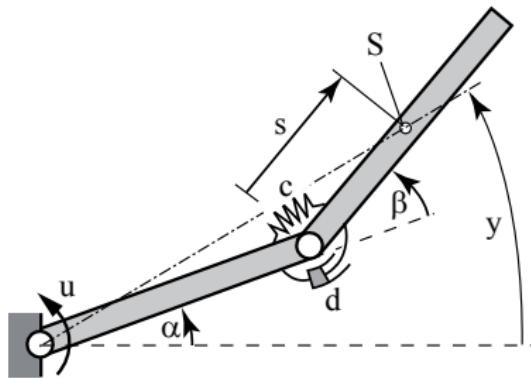
[Seifried, Blajer '13]

$$M = l^2 m \begin{bmatrix} \frac{5}{3} + \cos(\beta(t)) & \frac{1}{3} + \frac{1}{2} \cos(\beta(t)) \\ \frac{1}{3} + \frac{1}{2} \cos(\beta(t)) & \frac{1}{3} \end{bmatrix},$$

$$f_1 = \frac{1}{2} l^2 m \dot{\beta}(t) (2\dot{\alpha}(t) + \dot{\beta}(t)) \sin(\beta(t)),$$

$$f_2 = -c\beta(t) - d\dot{\beta}(t) - \frac{1}{2} l^2 m \dot{\alpha}(t)^2 \sin(\beta(t))$$

Rotational Manipulator Arm



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[Seifried, Blajer '13]

- relative degree = 2 (for $\cos(\beta) > 2/3$)
- internal dynamics: highly nonlinear, for $s/l > 2/3$ the linearized internal dynamics are unstable
- control: [B., Lanza '21]

Byrnes-Isidori form

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Byrnes-Isidori form

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Lie derivative:

- $(L_f h)(z) := h'(z)f(z)$
- $L_f^k h = L_f(L_f^{k-1} h)$ with $L_f^0 h = h$
- for $g(z) = [g_1(z), \dots, g_m(z)]$ we define

$$(L_g h)(z) := [(L_{g_1} h)(z), \dots, (L_{g_m} h)(z)]$$

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Relative degree r on $U \subseteq \mathbb{R}^n$:

- $\forall z \in U \forall k \in \{0, \dots, r-2\} : (L_g L_f^k h)(z) = 0_{m \times m}$
- $\forall z \in U : (L_g L_f^{r-1} h)(z) \in \mathbf{Gl}_m(\mathbb{R})$

Byrnes-Isidori form

$$\boxed{\begin{aligned}\dot{x}(t) &= f(x(t)) + g(x(t))u(t), \\ y(t) &= h(x(t))\end{aligned}}$$

\exists diffeomorphism $\Phi : U \rightarrow W$ s.t. $\begin{pmatrix} \xi(t) \\ \eta(t) \end{pmatrix} = \Phi(x(t))$, $\xi(t) \in \mathbb{R}^{rm}$, $\eta(t) \in \mathbb{R}^{n-rm}$
 transforms the system into **Byrnes-Isidori form**:

$$y(t) = \xi_1(t),$$

$$\dot{\xi}_1(t) = \xi_2(t),$$

$$\vdots$$

$$\dot{\xi}_{r-1}(t) = \xi_r(t),$$

$$\dot{\xi}_r(t) = (L_f^r h)(\Phi^{-1}(\xi(t), \eta(t))) + \Gamma(\Phi^{-1}(\xi(t), \eta(t)))u(t),$$

$$\dot{\eta}(t) = q(\xi(t), \eta(t)) + p(\xi(t), \eta(t))u(t)$$

Byrnes-Isidori form

$$\boxed{\begin{aligned}\dot{x}(t) &= f(x(t)) + g(x(t))u(t), \\ y(t) &= h(x(t))\end{aligned}}$$

$\text{im}(g(x))$ involutive:

$$\forall g_1, g_2 : \mathbb{R}^n \rightarrow \mathbb{R}^n \text{ with } g_i(x) \in \text{im}(g(x)) : [g_1, g_2](x) \in \text{im}(g(x)),$$

$$\text{where } [g_1, g_2](x) = g'_1(x)g_2(x) - g'_2(x)g_1(x)$$

$\implies p(\cdot) = 0$ in Byrnes-Isidori form [Isidori '95]

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internal dynamics: $\dot{\eta}(t) = q(\xi(t), \eta(t))$

Byrnes-Isidori form

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def. $T(y, \dots, y^{(r-1)})(t) := \begin{pmatrix} y(t) \\ \vdots \\ y^{(r-1)}(t) \\ \eta(t; \eta^0, y, \dots, y^{(r-1)}) \end{pmatrix}$

\implies Byrnes-Isidori form is equivalent to

$$\boxed{y^{(r)}(t) = F(T(y, \dots, y^{(r-1)})(t)) + G(T(y, \dots, y^{(r-1)})(t))u(t)}$$

with $F = (L_f^r h) \circ \Phi^{-1}$, $G = \Gamma \circ \Phi^{-1}$

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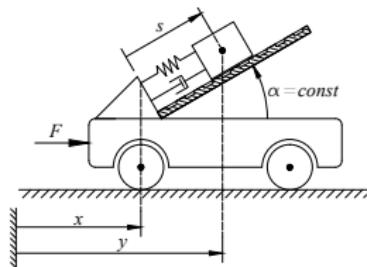
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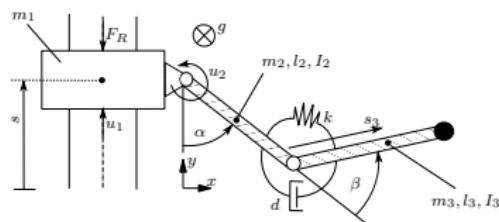
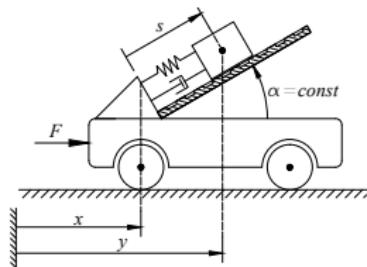
internal dynamics stable $\iff T$ is BIBO

Control of multibody systems – jointly with T. Reis and R. Seifried



[B., Lê, Reis '18]

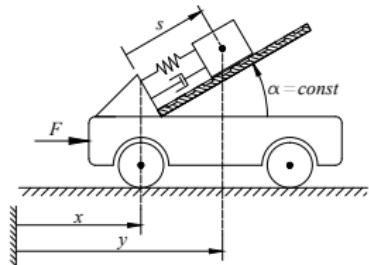
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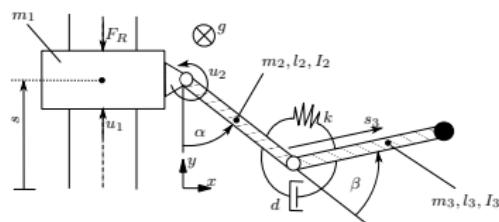
[B., Otto, Reis, Seifried '19]

[B., Lê, Reis '18]

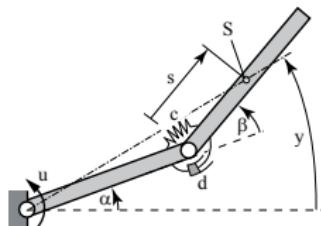
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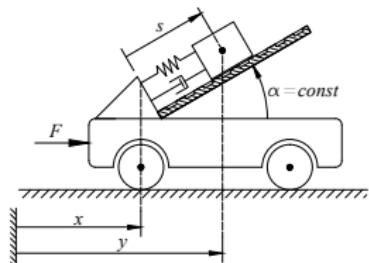


[B., Otto, Reis, Seifried '19]

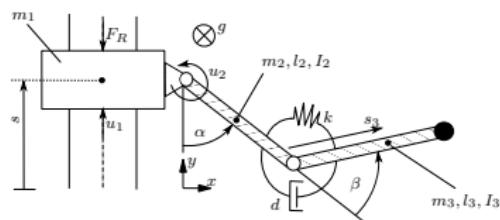


[B., Lanza '20]: unstable internal dynamics

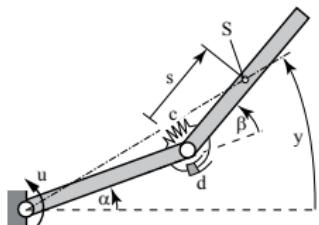
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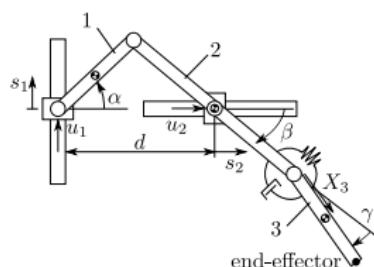
[B., Lê, Reis '18]



[B., Otto, Reis, Seifried '19]



[B., Lanza '20]: unstable internal dynamics



[B., Drücker, Lanza, Reis, Seifried '21]
unstable internal dynamics,
DAE formulation

Multibody systems in DAE formulation

$$\dot{q}(t) = v(t),$$

$$M(q(t))\dot{v}(t) = f(q(t), v(t)) + J(q(t))^{\top} \mu(t) + G(q(t))^{\top} \lambda(t) + B(q(t)) u(t),$$

$$0 = J(q(t))v(t) + j(q(t)),$$

$$0 = g(q(t)),$$

$$y(t) = h(q(t), v(t)),$$

with

- generalized mass matrix $M : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$,
- generalized forces $f : \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}^n$,
- holonomic constraints $g : \mathbb{R}^n \rightarrow \mathbb{R}^\ell$ and $G : \mathbb{R}^n \rightarrow \mathbb{R}^{\ell \times n}$,
- nonholonomic constraints $J : \mathbb{R}^n \rightarrow \mathbb{R}^{p \times n}$ and $j : \mathbb{R}^n \rightarrow \mathbb{R}^p$,
- input distribution matrix $B : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times m}$,
- output measurement function $h : \mathbb{R}^n \times \mathbb{R}^n \rightarrow \mathbb{R}^m$

Multibody systems in DAE formulation

$$\dot{x} = \begin{pmatrix} x_2 \\ M(x_1)^{-1}f(x_1, x_2) \end{pmatrix} + \begin{bmatrix} I_n & 0 \\ 0 & M(x_1)^{-1} \end{bmatrix} \begin{bmatrix} 0 & 0 & 0 \\ J(x_1)^\top & G(x_1)^\top & B(x_1) \end{bmatrix} u_{\text{aux}},$$

$$y_{\text{aux}} = H(x),$$

with $x_1 = q, x_2 = v$ and auxiliary inputs and outputs

$$u_{\text{aux}}(t) := \begin{pmatrix} \mu(t) \\ \lambda(t) \\ u(t) \end{pmatrix}, \quad y_{\text{aux}}(t) := H(q(t), v(t)) = \begin{pmatrix} J(q(t))v(t) + j(q(t)) \\ g(q(t)) \\ h(q(t), v(t)) \end{pmatrix}$$

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Idea:

- transform auxiliary ODE system into Byrnes-Isidori form
- add the constraints $y_{\text{aux},1} = 0$ and $y_{\text{aux},2} = 0$ afterwards to derive the internal dynamics of the original MBS

Multibody systems in DAE formulation

$$\dot{x} = \begin{pmatrix} x_2 \\ M(x_1)^{-1}f(x_1, x_2) \end{pmatrix} + \begin{bmatrix} I_n & 0 \\ 0 & M(x_1)^{-1} \end{bmatrix} \begin{bmatrix} 0 & 0 & 0 \\ J(x_1)^\top & G(x_1)^\top & B(x_1) \end{bmatrix} u_{\text{aux}},$$

$$y_{\text{aux}} = H(x),$$

with $x_1 = q, x_2 = v$ and auxiliary inputs and outputs

$$u_{\text{aux}}(t) := \begin{pmatrix} \mu(t) \\ \lambda(t) \\ u(t) \end{pmatrix}, \quad y_{\text{aux}}(t) := H(q(t), v(t)) = \begin{pmatrix} J(q(t))v(t) + j(q(t)) \\ g(q(t)) \\ h(q(t), v(t)) \end{pmatrix}$$

Idea:

- transform auxiliary ODE system into Byrnes-Isidori form
- add the constraints $y_{\text{aux},1} = 0$ and $y_{\text{aux},2} = 0$ afterwards to derive the internal dynamics of the original MBS

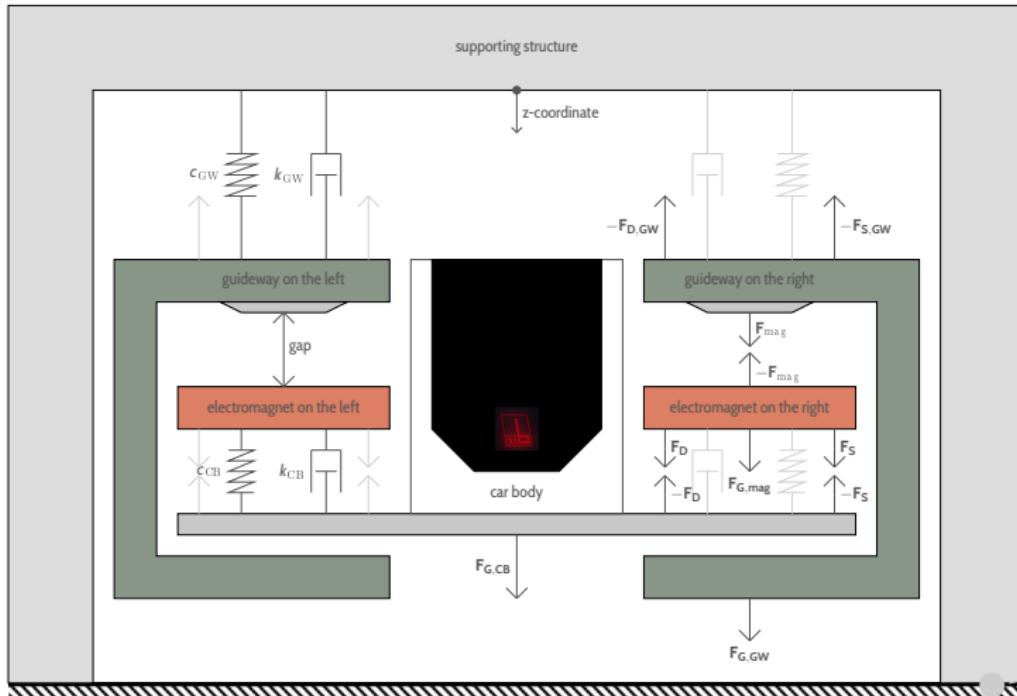
stability analysis without Byrnes-Isidori form: [Lanza '21]

Magnetic levitation system – cooperation with TU Ilmenau and Max Bögl



Bildquelle: <https://transportsystemboegl.com>, Pressemitteilung vom 26.04.2024

Magnetic levitation system – cooperation with TU Ilmenau and Max Bögl



Magnetic levitation system – cooperation with TU Ilmenau and Max Bögl

$$\dot{x}(t) = \begin{pmatrix} x_4(t) \\ x_5(t) \\ x_6(t) \\ \frac{1}{m_{\text{mag}}}(F_{G,\text{mag}} + F_{S,D}(x(t)) - F_{\text{mag}}(x(t))) \\ \frac{1}{m_{\text{CB}}}(F_{G,\text{CB}} - F_{S,D}(x(t))) \\ \frac{1}{m_{\text{GW}}}(F_{G,\text{GW}} - \tilde{F}_{S,D}(x(t)) + F_{\text{mag}}(x(t))) \\ -2RI_{\text{mag}}(x(t)) \end{pmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} u(t),$$

$$y(t) = x_1(t) - x_3(t)$$

Input: voltage at the electromagnet

[Oppeneiger, Lanza, Schell, Dennstädt, Schaller, Zamzow, B., Worthmann '24]:
 relative degree = 3 on $\{x_7 \neq 0\}$ and internal dynamics are stable

Magnetic levitation system – cooperation with TU Ilmenau and Max Bögl

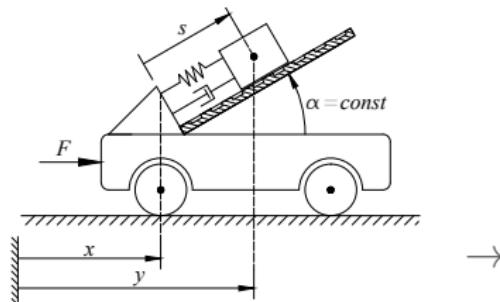
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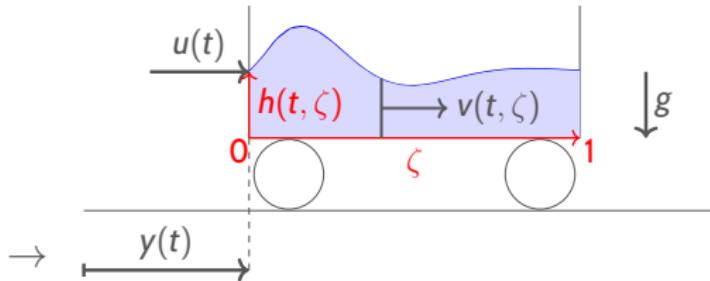
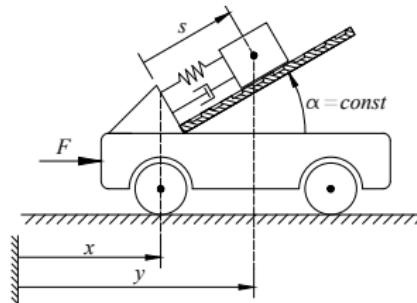
[Oppeneiger, Lanza, Schell, Dennstädt, Schaller, Zamzow, B., Worthmann '24]:
 relative degree = 3 on $\{x_7 \neq 0\}$ and internal dynamics are stable

Open problem: relative degree not well-defined everywhere



→

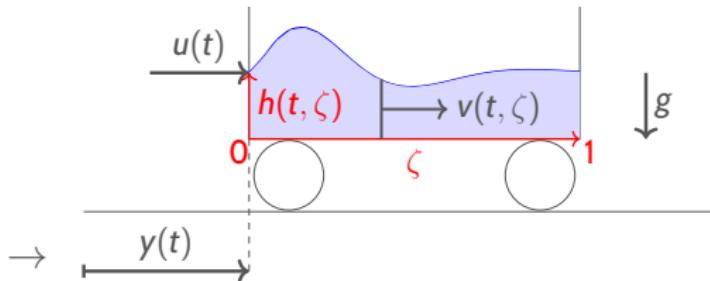
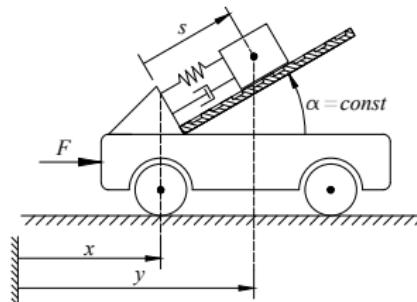
$$\ddot{y}(t) = T(y, \dot{y})(t) + \gamma u(t)$$



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$$\ddot{y}(t) = \hat{T}(y, \dot{y})(t) + \hat{\gamma} u(t)$$

[B., Puche, Schwenninger '22]



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[B., Puche, Schwenninger '22]

Finite and infinite dimensional systems in the same class!

Class of ∞ -dimensional systems

$$y^{(r)}(t) = F(T(y, \dots, y^{(r-1)})(t)) + G(T(y, \dots, y^{(r-1)})(t))u(t)$$

allows for a “simple” class of ∞ -dimensional systems
→ internal dynamics described by PDE

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 → internal dynamics described by PDE

$r = 1$: [Ilchmann, Ryan, Sangwin '02, etc.]

$$(Ty)(t) = A_1 y(t) + A_2 \int_0^t \mathcal{T}(t-s)A_3 y(s) \, ds$$

- $(\mathcal{T}(t))_{t \geq 0}$ exp. stable C^0 -semigroup on real Hilbert space X with generator $A_4 : \mathcal{D}(A_4) \subseteq X \rightarrow X$ (*finite dimensional*: $\mathcal{T}(t) = e^{A_4 t}$)
- (A_4, A_3, A_2) “regular well-posed”, $A_1 \in \mathbb{R}^{m \times m}$

Class of ∞ -dimensional systems

$$y^{(r)}(t) = F(T(y, \dots, y^{(r-1)})(t)) + G(T(y, \dots, y^{(r-1)})(t))u(t)$$

$r \in \mathbb{N}$: [Ilchmann, Selig, Trunk '16]

Byrnes-Isidori form for linear ∞ -dimensional systems

$$\dot{\eta}(t) = A_4\eta(t) + A_3y(t),$$

$$y^{(r)}(t) = R_1y(t) + \dots R_r y^{(r-1)}(t) + A_2\eta(t) + \gamma u(t)$$

Class of ∞ -dimensional systems

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Byrnes-Isidori form for linear ∞ -dimensional systems

$$\begin{aligned}\dot{\eta}(t) &= A_4\eta(t) + A_3y(t), \\ y^{(r)}(t) &= R_1y(t) + \dots R_r y^{(r-1)}(t) + A_2\eta(t) + \gamma u(t) \\ &= T(y, \dots, y^{(r-1)})(t) + \gamma u(t)\end{aligned}$$

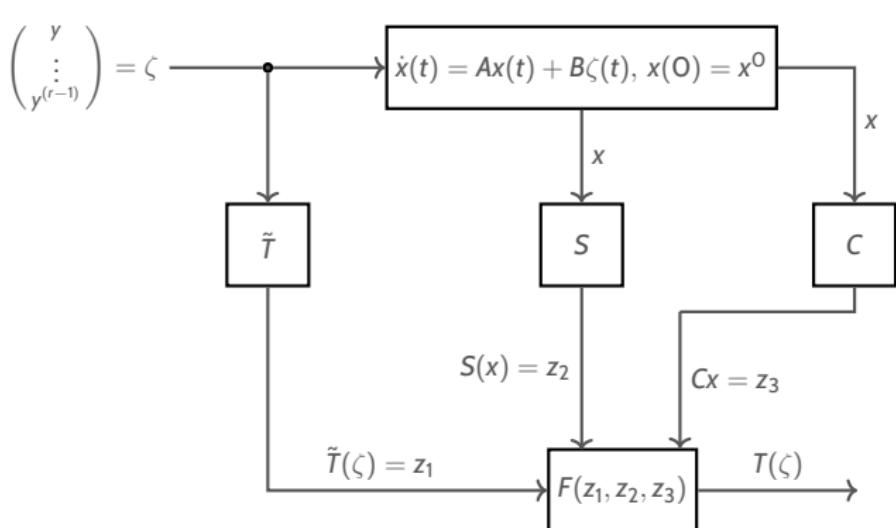
with $T(y, \dots, y^{(r-1)})(t)$

$$= R_1y(t) + \dots R_r y^{(r-1)}(t) + A_2 \int_0^t \mathcal{T}(t-s)A_3y(s) \, ds$$

Class of ∞ -dimensional systems

$$y^{(r)}(t) = F(T(y, \dots, y^{(r-1)})(t)) + G(T(y, \dots, y^{(r-1)})(t))u(t)$$

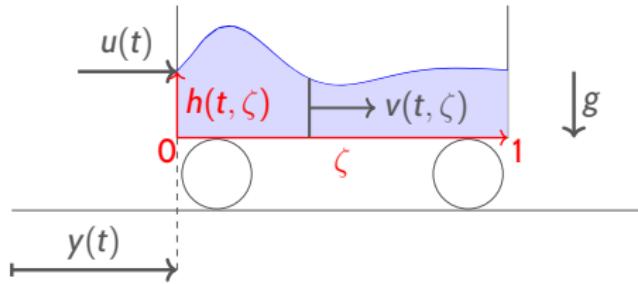
$r \in \mathbb{N}$: [B., Puche, Schwenninger '20]



- (A, B, C) regular well-posed
- $f \mapsto \mathcal{L}^{-1}(G) * f$ bounded
- S nonlinear, $\mathcal{D}(S) = X$, (A, B, S) BIBO stable

Rolling water tank – [B., Puche, Schwenninger '22]

$$\begin{aligned} \partial_t h + \partial_\zeta(hv) &= 0, \\ \partial_t v + \partial_\zeta \left(\frac{v^2}{2} + gh \right) \\ &\quad + hS\left(\frac{v}{h}\right) = -\ddot{y} \end{aligned}$$

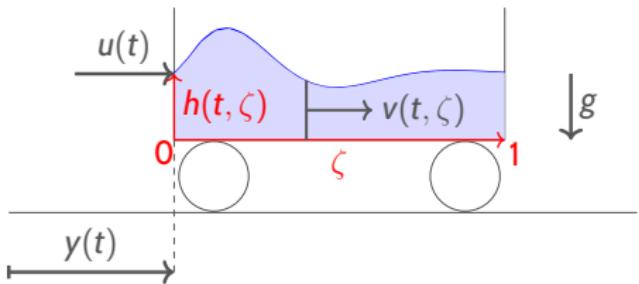


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Linearized model:

$$\partial_t z_1 = -h_0 \partial_\zeta z_2, \quad \partial_t z_2 = -g \partial_\zeta z_1 - \mu z_2 - \ddot{y}, \quad z_2(t, 0) = z_2(t, 1) = 0$$

$$\ddot{y}(t) = \frac{g}{2m_T} (z_1(t, 1) - z_1(t, 0)) (2h_0 + z_1(t, 1) + z_1(t, 0))$$

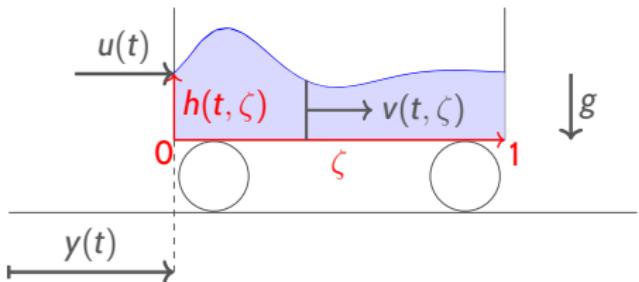
$$+ \frac{\mu h_0}{m_T} \int_0^1 z_2(t, \zeta) d\zeta + \frac{\mu}{m_T} \int_0^1 z_1(t, \zeta) z_2(t, \zeta) d\zeta + \frac{u(t)}{m_T}$$

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Linearized model:

$$\dot{z}(t) = Az(t) + Ab\dot{y}(t), \quad Az = - \begin{pmatrix} h_0 \partial_\zeta z_2 \\ g \partial_\zeta z_1 + \mu z_2 \end{pmatrix}, \quad b = \begin{pmatrix} 0 \\ -1 \end{pmatrix}$$

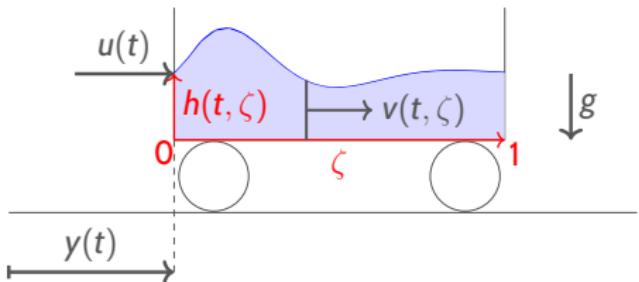
$$\begin{aligned} z_1(t, 1) - z_1(t, 0) &= Cz(t) = CT(t)z(0) + C \int_0^t T(t-s)Ab\dot{y}(s) ds \\ &= c(t) + ((\mathfrak{h}_{L^1} + \mathfrak{h}_\delta) * \dot{y})(t) \end{aligned}$$

Rolling water tank – [B., Puche, Schwenninger '22]

$$\partial_t h + \partial_\zeta(hv) = 0,$$

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$$\ddot{y}(t) = T(\dot{y})(t) + \frac{u(t)}{m_T}$$

Lemma: $\mathfrak{h}_\delta = \delta_0 + 2 \sum_{k \in \mathbb{N}} (-1)^k e^{-k\mu/\sqrt{h_0 g}} \delta_{k/\sqrt{h_0 g}}$ $\implies T$ is BIBO

“Hard” class of ∞ -dimensional systems

→ there is NO concept of relative degree

- boundary controlled heat equation [Reis, Selig '15]

$$\partial_t x(t) = \Delta x(t), \quad u(t) = (\nu^\top \cdot \nabla x(t))|_{\partial\Omega},$$

$$y(t) = \int_{\partial\Omega} x(t)(\zeta) d\zeta$$

- general class of boundary control problems based on m-dissipative operators [Puche, Reis, Schwenninger '21, Puche '19]

$$\dot{x}(t) = \mathfrak{A}x(t), \quad x(0) = x_0 \in \mathcal{D}(\mathfrak{A}) \subseteq X,$$

$$u(t) = \mathfrak{B}x(t), \quad y(t) = \mathfrak{C}x(t)$$

e.g. lossy transmission line, wave equation, diffusion equation

- Fokker-Planck equation [B. '21]

Monodomain equations [B., Breiten, Puche, Reis '21] – (simple) model for the electric activity of the human heart to describe defibrillation processes

$$\begin{aligned}\partial_t v(t) &= \nabla \cdot (D \nabla v(t)) + p_3(v)(t) - w(t) + I_{s,i}(t) + BI_{s,e}(t), \\ \partial_t w(t) &= cv(t) - dw(t), \quad y(t) = B'v(t)\end{aligned}$$

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Control objective: “reentry waves”, which can be interpreted as fibrillation processes, should be terminated

