

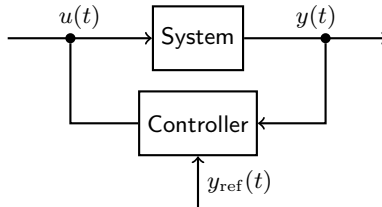
Funnel control for DAE systems

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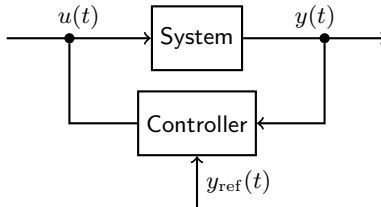
Munich, June 30, 2016

Adaptive Control



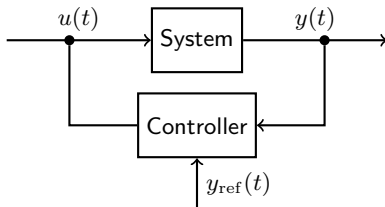
- no knowledge of system parameters, only “structure” of mathematical model for the system
- *aim*: design controller such that $y(t)$ “tracks” $y_{\text{ref}}(t)$

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Relative degree $r \in \mathbb{N}$

$$\dot{x}(t) = Ax(t) + bu(t), \quad y(t) = cx(t)$$

$$\dot{y}(t) = cAx(t) + cbu(t); \quad cb \neq 0 \Rightarrow r = 1$$

$$cb = 0 \Rightarrow \ddot{y}(t) = cA^2x(t) + cAbu(t); \quad cAb \neq 0 \Rightarrow r = 2$$

$$cAb = 0 \Rightarrow \dots$$

$$cb = cAb = \dots = cA^{r-2}b = 0 \wedge cA^{r-1}b \neq 0$$

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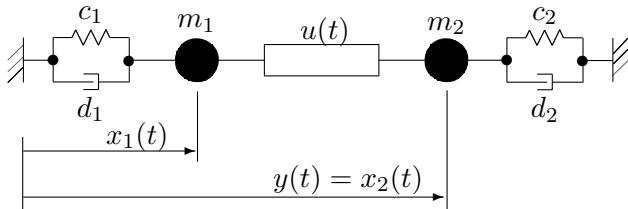


Figure: Mass-spring-damper system

Position control:

$$u(t) = x_2(t) - x_1(t)$$

$$\implies \text{relative degree} = 0$$

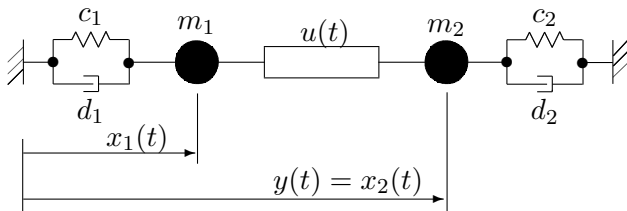


Figure: Mass-spring-damper system

Velocity control:

$$u(t) = \dot{x}_2(t) - \dot{x}_1(t)$$

$$\implies \text{relative degree} = 1$$

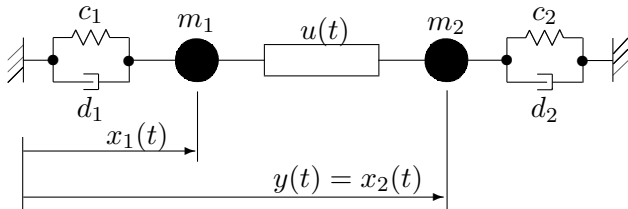


Figure: Mass-spring-damper system

Force control:

$$u(t) = M(\ddot{x}_2(t) - \ddot{x}_1(t))$$

$$\implies \text{relative degree} = 2$$

Zero dynamics

$$\dot{x}(t) = Ax(t) + bu(t), \quad y(t) = cx(t)$$

$$\mathcal{ZD} := \{ (x, u) \mid \dot{x}(t) = Ax(t) + bu(t), \quad 0 = cx(t) \}$$

$$\mathcal{ZD} \text{ stable} :\iff \forall (x, u) \in \mathcal{ZD} : \lim_{t \rightarrow \infty} (x(t), u(t)) = 0$$

Theorem:

$$\mathcal{ZD} \text{ stable} \iff \forall \lambda \in \overline{\mathbb{C}}_+ : \det \begin{bmatrix} A - \lambda I_n & b \\ c & 0 \end{bmatrix} \neq 0$$

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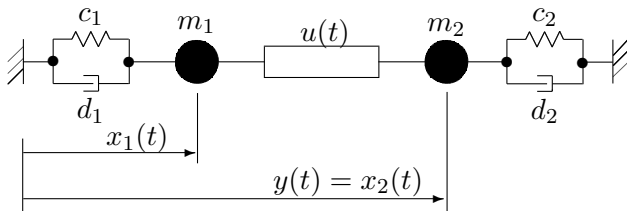


Figure: Mass-spring-damper system

Zero dynamics:

$$y(t) = 0 \quad \Rightarrow \quad x_2(t) = 0 \quad \Rightarrow \quad x_1(t) \rightarrow 0, \quad u(t) \rightarrow 0$$

ODE systems

$$\dot{x}(t) = f_1(x(t), y(t)), \quad x(0) = x^0, \quad (1)$$

$$\dot{y}(t) = f_2(y(t)) + f_3(x(t)) + \Gamma(y(t))u(t), \quad y(0) = y^0. \quad (2)$$

$x : \mathbb{R} \rightarrow \mathbb{R}^n$, $u, y : \mathbb{R} \rightarrow \mathbb{R}^m$; f_1, f_2, f_3 differentiable;
 $\Gamma : \mathbb{R}^m \rightarrow \mathbb{R}^{m \times m}$ differentiable

- (1) internal dynamics
- (2) input-output behavior

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relative degree:

$$\dot{z}(t) = f(z(t)) + g(z(t))u(t)$$

$$y(t) = h(z(t))$$

hat **strict relative degree** $r \in \mathbb{N} : \iff$ [ISIDORI '95]

- $\forall \xi \in \mathbb{R}^n \forall k = 0, \dots, r-2 : L_g L_f^k h(\xi) = 0,$
 $[L_f h = (\partial h / \partial z) f]$
- $\forall \xi \in \mathbb{R}^n : \det L_g L_f^{r-1} h(\xi) \neq 0.$

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(1), (2) has strict rel. deg. 1 $\iff \det \Gamma(y) \neq 0 \forall y \in \mathbb{R}^m$

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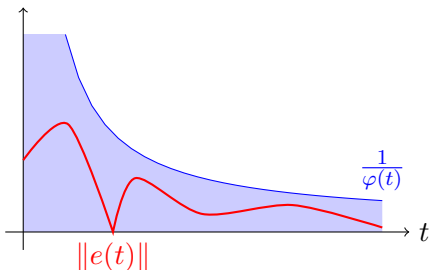
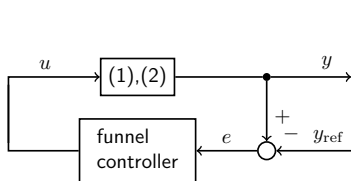
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$\mathcal{ZD}_{(1),(2)}$ stable, if (1) **input-to-state stable**: [SONTAG '89]

$$\forall (x^0, y) \quad \forall t \geq 0 : \|x(t; x^0, y)\| \leq \alpha(\|x^0\|, t) + \sup_{s \in [0, t]} \beta(\|y(s)\|),$$

$$\dot{x}(t) = f_1(x(t), y(t)), \quad x(0) = x^0, \quad (1)$$

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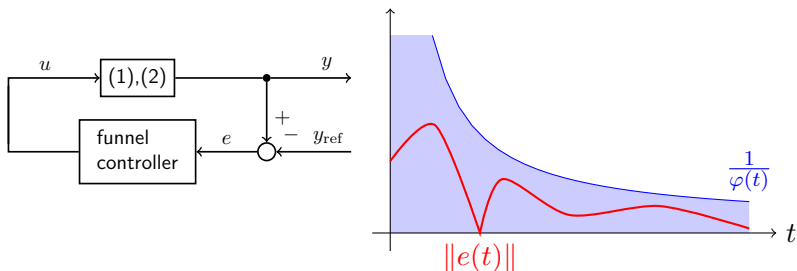


[ILCHMANN & RYAN '09]: funnel control works if

- strict relative degree 1 and “high-gain matrix” $\Gamma(y)$ pos. def. for all $y \in \mathbb{R}^m$
- (1) is ISS (zero dynamics are stable)

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$$\Downarrow$$

$$\dot{x}(t) = f_1(x(t), y(t)), \quad x(0) = x^0, \quad (3)$$

$$\tilde{\Gamma}(y(t)) \dot{y}(t) = f_2(y(t)) + f_3(x(t)) + u(t), \quad y(0) = y^0. \quad (4)$$

$\{(1), (2) \text{ with strict rel. deg. } 1\} \stackrel{\tilde{\Gamma}=\Gamma^{-1}}{\subseteq} \{(3), (4)\}$

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$$\dot{x}(t) = x(t) + y_1(t)$$

$$\begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{pmatrix} \dot{y}_1(t) \\ \dot{y}_2(t) \\ \dot{y}_3(t) \end{pmatrix} = \begin{pmatrix} 0 \\ y_2(t) \\ y_3(t) \end{pmatrix} + \begin{pmatrix} x(t) \\ 0 \\ 0 \end{pmatrix} + \begin{pmatrix} u_1(t) \\ u_2(t) \\ u_3(t) \end{pmatrix}$$

$$y_1 = u_1 - \dot{u}_1 \quad \Rightarrow \quad \int y_1 = \int u_1 - u_1$$

$$G(s) = \begin{bmatrix} s-1 & 0 & 0 \\ 0 & -1 & \\ 0 & 0 & \frac{1}{s-1} \end{bmatrix}, \quad \lim_{s \rightarrow \infty} \begin{bmatrix} s^{-1} & 0 & 0 \\ 0 & s^0 & 0 \\ 0 & 0 & s^1 \end{bmatrix} G(s) \in \mathbb{R}^{3 \times 3} \text{ inv.}$$

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Theorem [B., ILCHMANN, REIS '14]

$$\dot{x}(t) = f_1(x(t), y(t)), \quad x(0) = x^0, \quad (3)$$

$$\tilde{\Gamma}(y(t)) \dot{y}(t) = f_2(y(t)) + f_3(x(t)) + u(t), \quad y(0) = y^0. \quad (4)$$

- (3) is ISS
- $\tilde{\Gamma}(y) = RG(y)R^\top$, $G(y) > 0$
- f'_2 bounded on $\ker R^\top$
- \hat{k} "large enough"
- y^0 consistent

Then the *funnel controller*

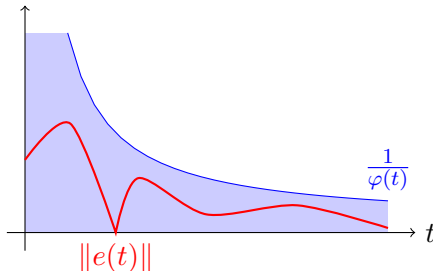
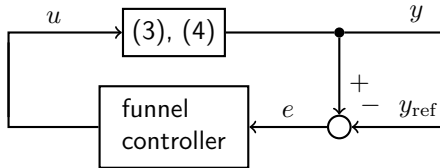
$$u(t) = -k(t) e(t), \quad \text{where} \quad e(t) = y(t) - y_{\text{ref}}(t)$$

$$k(t) = \hat{k} / (1 - \varphi(t)^2 \|e(t)\|^2),$$

achieves: $(x, y, k) \in L^\infty$, $\wedge \exists \varepsilon > 0 \forall t > 0 : \|e(t)\| \leq \varphi(t)^{-1} - \varepsilon$

$$\dot{x}(t) = f_1(x(t), y(t)), \quad x(0) = x^0, \quad (3)$$

$$\tilde{\Gamma}(y(t)) \dot{y}(t) = f_2(y(t)) + f_3(x(t)) + u(t), \quad y(0) = y^0. \quad (4)$$



Comparison of ODEs and DAEs

$$\dot{x}(t) = f_1(x(t), y(t)), \quad x(0) = x^0, \quad (1)$$

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ODEs	DAEs
(1) is ISS	(3) is ISS
$\Gamma > 0$ (rel. deg. 1)	$\tilde{\Gamma} \geq 0$ (mixed rel. deg.)
$\hat{k} = 1$	\hat{k} "large enough"
$y^0 \in \mathbb{R}^m$	y^0 consistent

Electrical circuits

$$\boxed{\frac{d}{dt}Ex(t) = Ax(t) + Bu(t), \quad y(t) = Cx(t)} \quad u = \begin{pmatrix} i_{\mathcal{I}} \\ v_{\mathcal{V}} \end{pmatrix}, \quad y = \begin{pmatrix} -v_{\mathcal{I}} \\ -i_{\mathcal{V}} \end{pmatrix}$$

$$sE - A = \begin{bmatrix} sA_{\mathcal{C}}CA_{\mathcal{C}}^{\top} + A_{\mathcal{R}}GA_{\mathcal{R}}^{\top} & A_{\mathcal{L}} & A_{\mathcal{V}} \\ -A_{\mathcal{L}}^{\top} & s\mathcal{L} & 0 \\ -A_{\mathcal{V}}^{\top} & 0 & 0 \end{bmatrix}, \quad B = C^{\top} = \begin{bmatrix} -A_{\mathcal{I}} & 0 \\ 0 & 0 \\ 0 & -I_{n_{\mathcal{V}}} \end{bmatrix}$$

- $A_{\mathcal{C}}, A_{\mathcal{R}}, A_{\mathcal{L}}, A_{\mathcal{V}}, A_{\mathcal{I}}$ – element-related incidence matrices
 $\mathcal{C}, \mathcal{G}, \mathcal{L}$ – constitutive relations of capacitances, resistances and inductances

passivity: $\mathcal{C} = \mathcal{C}^{\top} > 0, \mathcal{L} = \mathcal{L}^{\top} > 0, \mathcal{G} + \mathcal{G}^{\top} > 0$

Theorem [B., REIS '14]

$[E, A, B, C]$ MNA model of a circuit; assume one of the following:

- neither IL -loops, nor VC -cutsets except for VC -cutsets with at least one inductor
- neither VC -cutsets, nor IC -loops except for IC -loops with at least one capacitor

$\implies \mathcal{ZD}$ are stable.

Theorem [B., REIS '14]

- $[E, A, B, C]$ MNA model of a circuit with stable \mathcal{ZD}

Then the *funnel controller*

$$\begin{array}{l}
 u(t) = -k(t) e(t), \quad \text{where} \quad e(t) = y(t) - y_{\text{ref}}(t) \\
 k(t) = \frac{1}{1 - \varphi(t)^2 \|e(t)\|^2},
 \end{array}$$

applied to $[E, A, B, C]$ achieves that

$$x \in L^\infty, k \in L^\infty \quad \wedge \quad \exists \varepsilon > 0 \quad \forall t > 0 : \|e(t)\| \leq \varphi(t)^{-1} - \varepsilon.$$

$$E\dot{x}(t) = Ax(t) + Bu(t)$$

$$y(t) = Cx(t)$$

