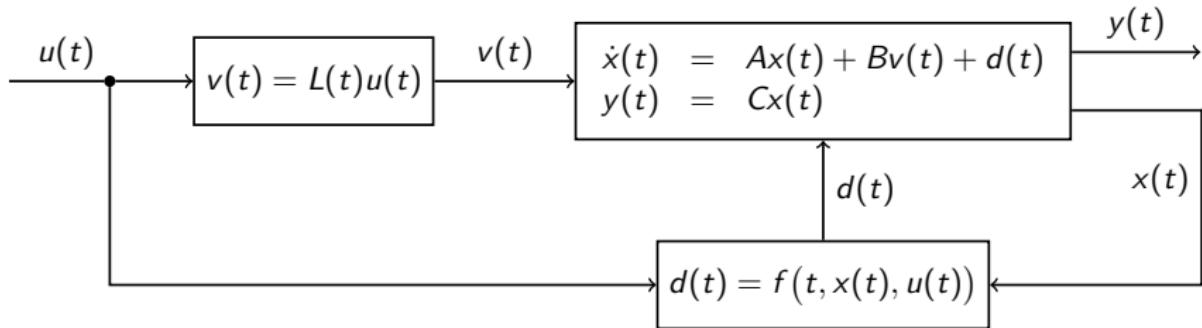




THOMAS BERGER

Fault tolerant funnel control

Linear systems with uncertainties and actuator faults

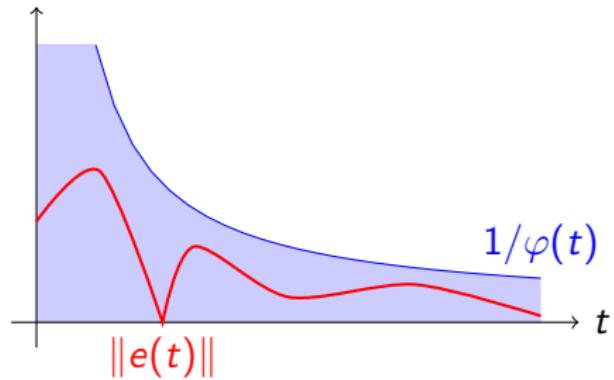
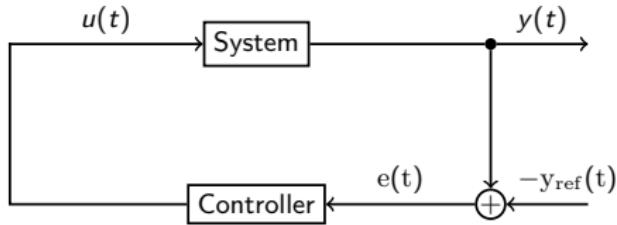


- $A \in \mathbb{R}^{n \times n}$, $B \in \mathbb{R}^{n \times m}$, $C \in \mathbb{R}^{p \times n}$, $m \geq p$
- f continuous and bounded (*modelling errors, uncertainties, disturbances, actuator saturation, etc.*)
- $L \in \mathcal{C}^\infty(\mathbb{R} \rightarrow \mathbb{R}^{m \times m})$ s.t. $L, \dot{L}, \dots, L^{(n)}$ bounded (*reliability of actuators*)

$$\dot{x}(t) = Ax(t) + BL(t)u(t) + f(t, x(t), u(t)), \quad y(t) = Cx(t)$$

- $\text{rk } BL(t) = q \geq p$ (e.g. *q groups of actuators which perform the same control task; in each at least one (partially) functional*)
typical: $q = p$
- $CA^k BL(\cdot) = 0, CA^k f(\cdot) = 0$ for all $k = 0, \dots, r - 2$
- $\Gamma := CA^{r-1}B \in \mathbb{R}^{p \times m}$ satisfies $\text{rk } \Gamma L(t) = p$ for all $t \in \mathbb{R}$

Control objective



$$\Phi_r = \left\{ \varphi \in \mathcal{C}^r(\mathbb{R}_{\geq 0} \rightarrow \mathbb{R}) \mid \begin{array}{l} \varphi, \dot{\varphi}, \dots, \varphi^{(r)} \text{ bounded,} \\ \varphi(\tau) > 0 \text{ for all } \tau > 0, \\ \text{and } \liminf_{\tau \rightarrow \infty} \varphi(\tau) > 0 \end{array} \right\}$$

Theorem [B. '17] - EXT. OF [ILCHMANN & MÜLLER '07]

\exists Lyapunov transf. U (under mild conditions)

$$\text{s.t. } (\hat{A}, \hat{B}, \hat{C}) := \left((UA + \dot{U})U^{-1}, UBL, CU^{-1} \right),$$

$$\hat{f}(t, z, u) := U(t)f\left(t, U(t)^{-1}z, u\right)$$

have the form

$$\hat{A}(t) = \begin{bmatrix} 0 & I_p & 0 & \cdots & 0 & 0 \\ 0 & 0 & I_p & & & \\ \vdots & \vdots & \ddots & \ddots & & \vdots \\ 0 & 0 & \cdots & 0 & I_p & 0 \\ R_1(t) & R_2(t) & \cdots & R_{r-1}(t) & R_r(t) & S(t) \\ P_1(t) & P_2(t) & \cdots & P_{r-1}(t) & P_r(t) & Q(t) \end{bmatrix}, \quad \hat{B}(t) = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ \Gamma L(t) \\ N(t) \end{bmatrix}, \quad \hat{f} = \begin{pmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ f_r \\ f_\eta \end{pmatrix},$$
$$\hat{C} = [I_p \ 0 \ \cdots \ 0]$$

$$\hat{A}(t) = \begin{bmatrix} 0 & I_p & 0 & \cdots & 0 & 0 \\ 0 & 0 & I_p & & & \\ \vdots & \vdots & \ddots & \ddots & & \vdots \\ 0 & 0 & \cdots & 0 & I_p & 0 \\ R_1(t) & R_2(t) & \cdots & R_{r-1}(t) & R_r(t) & S(t) \\ P_1(t) & P_2(t) & \cdots & P_{r-1}(t) & P_r(t) & Q(t) \end{bmatrix}, \quad \hat{B}(t) = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ \Gamma L(t) \\ N(t) \end{bmatrix}, \quad \hat{f} = \begin{pmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ f_r \\ f_\eta \end{pmatrix},$$
$$\hat{C} = [I_p \ 0 \ \cdots \ 0]$$

$$(\operatorname{rk} BL(t) =) \ q = p \implies P_2 = \dots = P_r = 0 \wedge N = 0$$

Transformation: $(y(t), \dot{y}(t), \dots, y^{(r-1)}(t), \eta(t)) := U(t)x(t)$

$$\begin{aligned} \implies y^{(r)}(t) &= \sum_{i=1}^r R_i(t)y^{(i-1)}(t) + S(t)\eta(t) + \Gamma L(t)u(t) \\ &\quad + f_r(t, y(t), \dots, y^{(r-1)}(t), \eta(t), u(t)), \\ \dot{\eta}(t) &= \sum_{i=1}^r P_i(t)y^{(i-1)}(t) + Q(t)\eta(t) + N(t)u(t) \\ &\quad + f_\eta(t, y(t), \dots, y^{(r-1)}(t), \eta(t), u(t)) \end{aligned}$$

Transformation: $(y(t), \dot{y}(t), \dots, y^{(r-1)}(t), \eta(t)) := U(t)x(t)$

$$\begin{aligned} \implies y^{(r)}(t) &= \sum_{i=1}^r R_i(t)y^{(i-1)}(t) + S(t)\eta(t) + \underbrace{\Gamma L(t)u(t)}_{>0} \\ &\quad + \cancel{f_r(t, y(t), \dots, y^{(r-1)}(t), \eta(t), u(t))}, \\ \dot{\eta}(t) &= \sum_{i=1}^r P_i(t)y^{(i-1)}(t) + \underbrace{Q(t)\eta(t)}_{\text{exp. st.}} + \cancel{N(t)u(t)} \\ &\quad + \cancel{f_\eta(t, y(t), \dots, y^{(r-1)}(t), \eta(t), u(t))} \end{aligned}$$

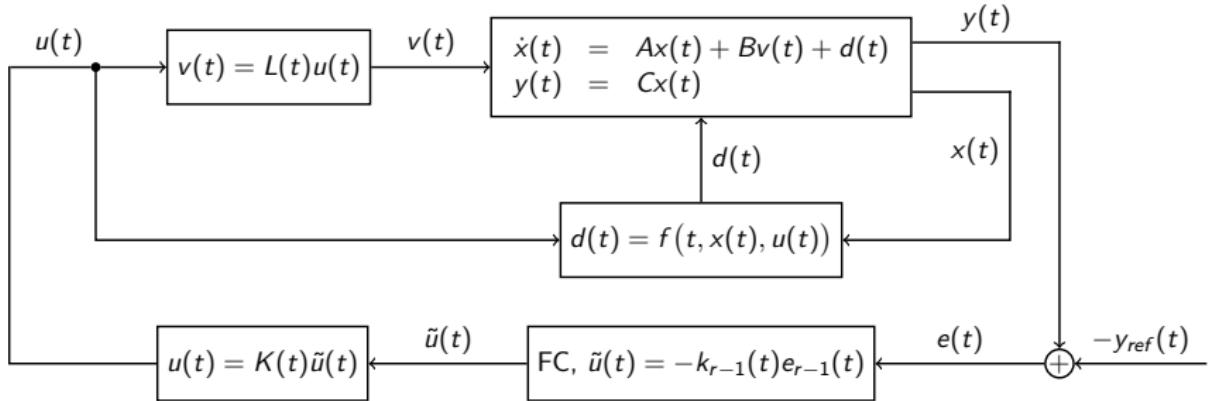
Funnel controller for systems with known relative degree $r \in \mathbb{N}$

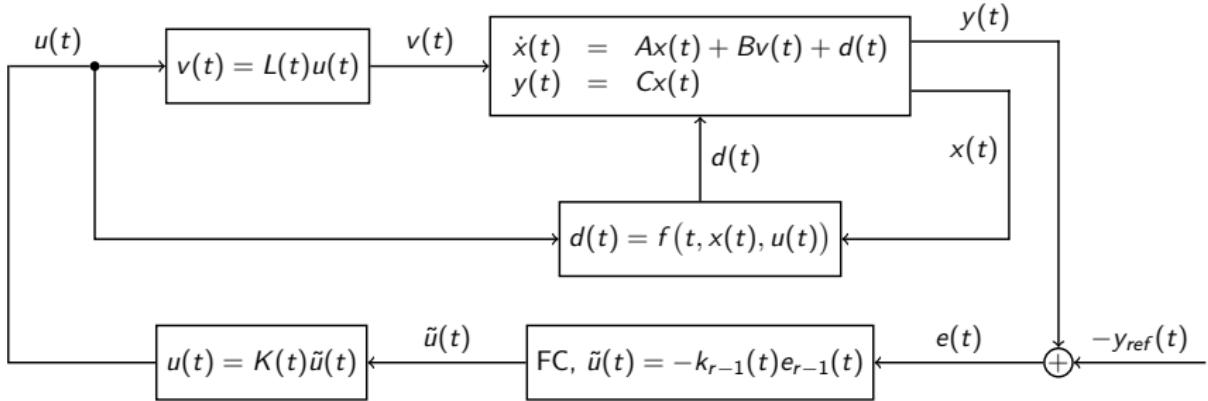
$$\begin{aligned} e_0(t) &= e(t) = y(t) - y_{ref}(t), \\ e_1(t) &= \dot{e}_0(t) + k_0(t) e_0(t), \\ e_2(t) &= \dot{e}_1(t) + k_1(t) e_1(t), \\ &\vdots \\ e_{r-1}(t) &= \dot{e}_{r-2}(t) + k_{r-2}(t) e_{r-2}(t), \\ k_i(t) &= 1/(1 - \varphi_i(t)^2 \|e_i(t)\|^2), \quad i = 0, \dots, r-1 \\ u(t) &= -k_{r-1}(t) e_{r-1}(t) \end{aligned}$$

Theorem [B., HOANG, REIS '18]

$y_{ref} \in \mathcal{W}^{r,\infty}$, $\varphi_i \in \Phi_{r-i}$, $\varphi_i(0) \|e_i(0)\| < 1 \implies u, k_i, y^{(i)}, \eta \in L^\infty$
and

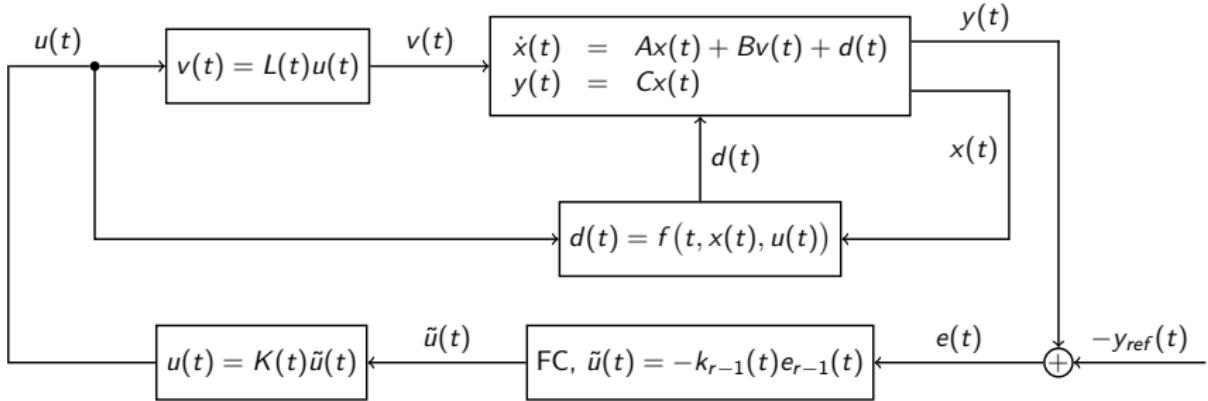
$$\|e_i(t)\| \leq \varphi_i(t)^{-1} - \varepsilon_i$$





$$u(t) = -k_{r-1}(t)K(t)e_{r-1}(t)$$

$$y^{(r)}(t) = \sum_{i=1}^r R_i(t)y^{(i-1)}(t) + S(t)\eta(t) + \textcolor{red}{\Gamma L(t)K(t)\tilde{u}(t)} + f_r$$
$$\dot{\eta}(t) = \sum_{i=1}^r P_i(t)y^{(i-1)}(t) + Q(t)\eta(t) + \textcolor{red}{N(t)K(t)\tilde{u}(t)} + f_\eta$$



$$u(t) = -k_{r-1}(t)K(t)e_{r-1}(t)$$

for controller weight matrix $K \in \mathcal{C}^\infty(\mathbb{R} \rightarrow \mathbb{R}^{m \times p})$ with

- $\exists \alpha > 0 : \Gamma L(t)K(t) + (\Gamma L(t)K(t))^\top \geq \alpha I_p,$
- $N(t)K(t) = 0$

$$\dot{x}(t) = Ax(t) + BL(t)u(t) + f(t, x(t), u(t)), \quad y(t) = Cx(t)$$

Theorem [B. '17]

- U is a Lyapunov transformation
- $\dot{\eta}(t) = Q(t)\eta(t)$ is uniformly exponentially stable (min. phase)
- $\exists \alpha > 0 : \Gamma L(t)K(t) + (\Gamma L(t)K(t))^\top \geq \alpha I_p$
- $N(t)K(t) = 0$
- $y_{ref} \in \mathcal{W}^{r,\infty}, \varphi_i \in \Phi_{r-i}, \varphi_i(0)\|e_i(0)\| < 1$

$\implies u, k_i, x \in L^\infty$ and

$$\|e_i(t)\| \leq \varphi_i(t)^{-1} - \varepsilon_i$$

Choice of $K(t)$

$q > p$: Only possible when system parameters and L are known!

Choice of $K(t)$

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$q = p$: Recall: $N(t) = 0$;
choose $K(t) = \Gamma^\top$ and assume that

$$\Gamma(L(t) + L(t)^\top)\Gamma^\top \geq \alpha I_p$$

→ there are at least p lin. ind. actuators, the reliability of which does not converge to 0;

Advantage: only Γ must be known

Example: Lateral motion of a Boeing 737 aircraft (linearized); taken from [TAO ET AL. '04]

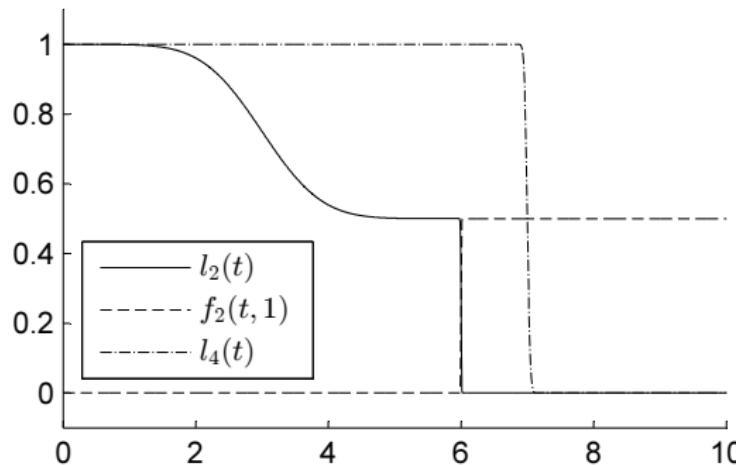
$$A = \begin{bmatrix} -0.13858 & 14.326 & -219.04 & 32.167 & 0 \\ -0.02073 & -2.1692 & 0.91315 & 0.000256 & 0 \\ 0.00289 & -0.16444 & -0.15768 & -0.00489 & 0 \\ 0 & 1 & 0.00618 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \end{bmatrix},$$
$$B = \begin{bmatrix} 0.15935 & 0.15935 & 0.00211 & 0.00211 \\ 0.01264 & 0.01264 & 0.21326 & 0.21326 \\ -0.12879 & -0.12879 & 0.00171 & 0.00171 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}, \quad C = \begin{bmatrix} 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

$$x = (v_b, p_b, r_b, \phi, \psi)^\top, \quad u = (d_{r1}, d_{r2}, d_{a1}, d_{a2})^\top$$

- v_b - lateral velocity
- p_b - roll rate
- r_b - yaw rate
- ϕ - roll angle
- ψ - yaw angle
- $d_{r1} + d_{r2}$ - rudder position
- $d_{a1} + d_{a2}$ - aileron position

$$L(t) = \text{diag} (1, l_2(t), 1, l_4(t)), \quad f(t, u) = B \begin{pmatrix} 0 \\ f_2(t, u_2) \\ 0 \\ 0 \end{pmatrix}$$

- d_{r2} : slowly decreasing efficiency to 50% on $[0, 6]$; at $t = 6$ additional fault which leads to actuator saturation by 1
- d_{a2} : sudden total fault at $t = 7$



$$y_{ref,1}(t) = 2 \sin t, \quad y_{ref,2}(t) = \cos t, \quad x(0) = 0,$$

$$\varphi_0(t) = (5e^{-t} + 0.1)^{-1}, \quad \varphi_1(t) = \left(\frac{5}{2}e^{-\frac{1}{2}t} + 0.1\right)^{-1},$$

$$K(t) = \Gamma^\top = \begin{bmatrix} 0.01184 & -0.12879 \\ 0.01184 & -0.12879 \\ 0.21327 & 0.00171 \\ 0.21327 & 0.00171 \end{bmatrix}$$

